

Sol. # 1

Jones matrix  $\begin{pmatrix} 1 & i \\ -i & 1 \end{pmatrix} \equiv M$

(i) For full transmission

$$(M) \begin{pmatrix} A \\ B \end{pmatrix} = \lambda \begin{pmatrix} A \\ B \end{pmatrix} \rightarrow \begin{pmatrix} 1 & i \\ -i & 1 \end{pmatrix} \begin{pmatrix} A \\ B \end{pmatrix} = \lambda \begin{pmatrix} A \\ B \end{pmatrix}$$

$$\rightarrow \begin{pmatrix} A + iB = \lambda A \\ -iA + B = \lambda B \end{pmatrix} \rightarrow \begin{vmatrix} 1 - \lambda & i \\ -i & 1 - \lambda \end{vmatrix} = 0$$

$$(1 - \lambda)^2 - 1 = 0 \rightarrow 1 - 2\lambda + \lambda^2 - 1 = 0$$

$$\rightarrow \lambda(\lambda - 2) = 0 \quad \therefore \lambda = 0 \text{ \& } 2.$$

For  $\lambda = 2$ ,

$$\begin{pmatrix} A + iB = 2A \\ -iA + B = 2B \end{pmatrix} \rightarrow \begin{pmatrix} -A + iB = 0 \\ -iA - B = 0 \end{pmatrix} \rightarrow \begin{pmatrix} -A + iB = 0 \\ A - iB = 0 \end{pmatrix}$$

$$\therefore A = iB$$

The Jones vector is

$$\underline{\underline{\begin{pmatrix} 1 \\ -i \end{pmatrix}}}$$

$$\begin{pmatrix} i \\ 1 \end{pmatrix} = i \begin{pmatrix} 1 \\ -i \end{pmatrix}$$

↳ right circularly polarized!

(ii) For zero transmission,

$$\begin{pmatrix} 1 & i \\ -i & 1 \end{pmatrix} \begin{pmatrix} A \\ B \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \end{pmatrix}$$

$$\rightarrow \begin{cases} A + iB = 0 \\ -iA + B = 0 \end{cases} \rightarrow B = iA$$

$$\underline{\underline{A = -iB}}$$

$$\begin{pmatrix} -i \\ 1 \end{pmatrix} = -i \underline{\underline{\begin{pmatrix} 1 \\ i \end{pmatrix}}}$$

$\therefore$  Jones vector is

$$\underline{\underline{\begin{pmatrix} 1 \\ +i \end{pmatrix}}}$$

↳ left circularly polarized!

Sol. # 2

(i) From Eq. (2.57),  $r_p = 0$  (TM mode)

$$r_p = -\frac{\tan(\theta_i - \phi)}{\tan(\theta_i + \phi)} = 0 \quad ; \quad \phi = \theta_t$$

Due to Snell's law ( $n_1 \sin \theta_i = n_2 \sin \phi$ ),  $\theta_i \neq \phi$  due to  $n_1 \neq n_2$ .

$\therefore \tan(\theta_i + \phi) = \infty$  to make  $r_p = 0$ .

$\rightarrow \theta_i + \phi = \frac{\pi}{2} \quad \therefore$  The angle between reflected and transmitted beams is a right angle.

(ii) From Eq. (2.59),

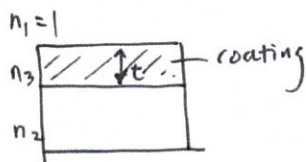
$$r_p = \frac{-n^2 \cos \theta + \sqrt{n^2 - \sin^2 \theta}}{n^2 \cos \theta + \sqrt{n^2 - \sin^2 \theta}} \quad ; \quad n = \frac{n_2}{n_1} \quad \left( \begin{array}{c} \theta_i \quad \theta_r = \theta_i \\ \theta_t \\ n_1 \\ n_2 \end{array} \right)$$

For normal incidence,  $\theta = 0$ .

$$\therefore r_p = \frac{-n^2 + n}{n^2 + n} = \frac{-n + 1}{n + 1}$$

$$R_p = |r_p|^2 = \left( \frac{-n + 1}{n + 1} \right)^2 = \left( \frac{n - 1}{n + 1} \right)^2 = \left( \frac{0.5}{2.5} \right)^2 = \underline{\underline{0.04}}$$

(iii)



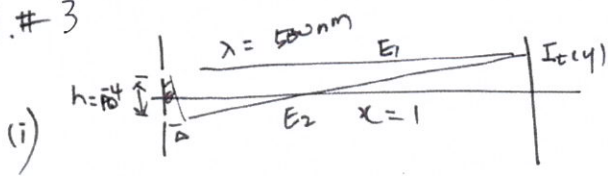
From Eq. (4.32)

$$r = \frac{n_3(1 - n_2) \cos kt - i(n_2 - n_3^2) \sin kt}{n_3(1 + n_2) \cos kt - i(n_2 + n_3^2) \sin kt}$$

for  $t = \frac{\pi}{2k}$ ,

$$\cos kt = 0 \quad \& \quad \sin kt = 1. \quad \therefore r = \frac{n_2 - n_3^2}{n_2 + n_3^2} \rightarrow \underline{\underline{R = \left( \frac{n_2 - n_3^2}{n_2 + n_3^2} \right)^2}}$$

Sol. # 3



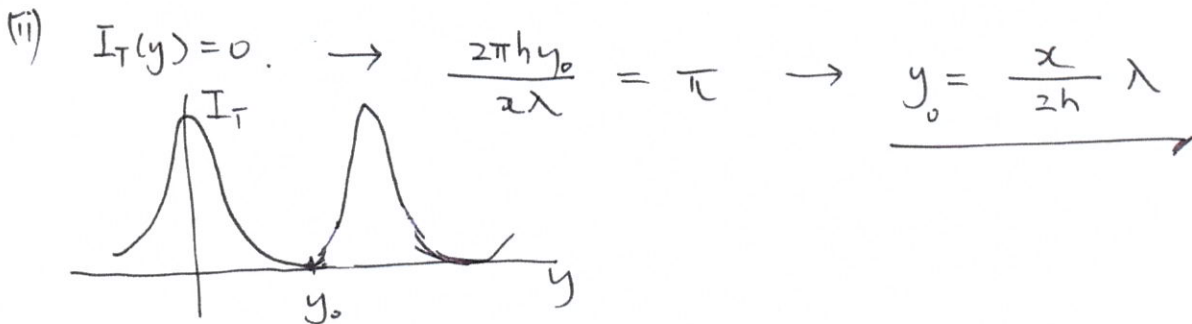
$$\Delta = h \sin \theta \approx h \tan \theta = \frac{hy}{x}$$

$$E_T = E_1 + E_2 = E_0 (1 + e^{i k \Delta}) e^{i(kx - \omega t)}$$

$$I_T = |E_T|^2 = I_0 (1 + e^{i k \Delta}) (1 + e^{-i k \Delta}) = I_0 (1 + 1 + e^{i k \Delta} + e^{-i k \Delta}) = 2 I_0 (1 + \cos k \Delta)$$

$$\therefore I_T(y) = 2 I_0 \left( 1 + \cos \frac{khy}{x} \right) \quad I_0 = |E_0|^2$$

$$= 2 I_0 \left[ 1 + \cos \left( \frac{2\pi hy}{x\lambda} \right) \right]$$



(iii) The energy is the concept of average in time.

$$\langle I_T \rangle = \frac{1}{Y} \int_0^Y I_T dy = 2 I_0, \text{ where } \int \cos \left( \frac{2\pi hy}{x\lambda} \right) dy = 0.$$

This satisfies the energy conservation law!

Sol. # 4

$$(i) R = |r|^2 = \frac{(n_T - n_i)^2}{(n_T + n_i)^2} = \left( \frac{1.52 - 1.35}{1.52 + 1.35} \right)^2 = 8.2 \times 10^{-3}$$

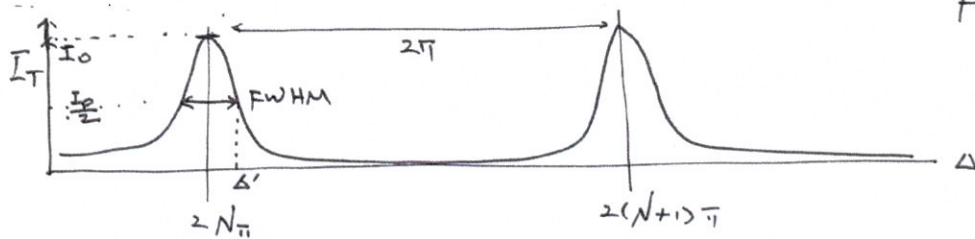
$$(ii) \text{ For } R=0, \quad \underline{n_T = \underline{n_i}}$$

Sol. # 5

From Eq. (4.8)

$$\bar{I}_T = \bar{I}_0 \frac{T^2}{(1-R)^2} \frac{1}{1 + F \sin^2 \frac{\Delta}{2}} \Rightarrow \bar{I}_0 \frac{1}{1 + F \sin^2 \frac{\Delta}{2}},$$

$$F = \frac{4R}{(1-R)^2}$$



$$\text{For FWHM, } \bar{I}_T = \frac{1}{2} \bar{I}_0 \rightarrow F \sin^2 \frac{\Delta'}{2} = 1$$

Because FWHM is 1% of  $2\pi$ ,

$$\Delta' = \frac{\text{FWHM}}{2} = 0.01 \times 2\pi \rightarrow \sin^2 \frac{\Delta'}{2} = \sin^2 \frac{(0.01 \times 2\pi)}{2}$$

$$= \sin^2 (0.0314)$$

$$= \sin^2 (1.8^\circ)$$

$$\doteq 0.001$$

$$\left( \begin{array}{l} 0.0314 : \pi = x : 180 \\ x = \frac{(0.0314)(180)}{\pi} = 1.8^\circ \end{array} \right)$$

$$\therefore F = 1000$$

$$\text{From } F = \frac{4R}{(1-R)^2} = 1000 \rightarrow (1 - 2R + R^2) \cdot 1000 = 4R$$

$$\rightarrow 1000R^2 - 2004R + 1000 = 0$$

$$\therefore R = \frac{2004 \pm \sqrt{2004^2 - 4000000}}{2000}$$

$$\doteq \frac{2004 \pm 126}{2000}$$

$$\therefore R = 0.939$$