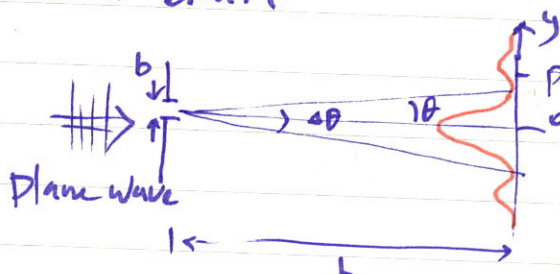


< Resolution >

- Diffraction limit

①

• Single slit



$$\beta = \frac{1}{2} k b \sin \theta$$

$$E_p = E_0 \operatorname{sinc}(\beta) e^{i(kr_0 - \omega t)}$$

$$I_p = I_0 \operatorname{sinc}^2(\beta)$$

For minima, $\sin \beta = 0 \rightarrow \beta = m\pi, m=0, \pm 1, \pm 2, \dots$

$$= \frac{1}{2} k b \sin \theta_m$$

$$= \frac{\pi b \sin \theta_m}{\lambda}$$

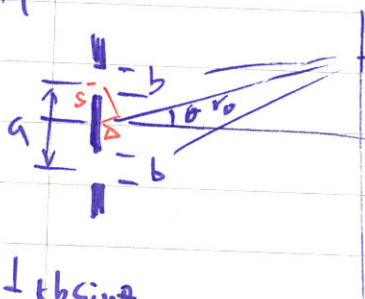
$$y_{\min} = L \sin \theta_m = \frac{m \lambda L}{b}$$

$$L_{\min} = \frac{b^2}{\lambda}, \text{ where } L \geq b.$$

$$\theta_{\min} = 2 \sin \theta_m = \frac{2\lambda}{b}$$

②

• Double slit



$$E_p = \frac{E_0}{r} e^{i(kr_0 - \omega t)} \left(\int_{-b/2}^{b/2} e^{i\Delta} ds \right)$$

$$\Delta = k s \sin \theta$$

$$\beta = \frac{1}{2} k b \sin \theta$$

$$\alpha = \frac{1}{2} k a \sin \theta$$

$$\frac{\sin \beta}{\beta} \cos \alpha$$

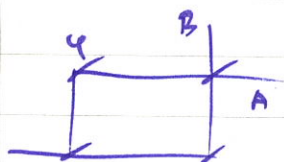
$$\therefore I_p = I_0 \frac{\sin^2(\beta)}{\beta^2} \cos^2(\alpha)$$

• Airy disk, $\theta = 1.22 \frac{\lambda}{b} \leftarrow (\text{diameter})$

③

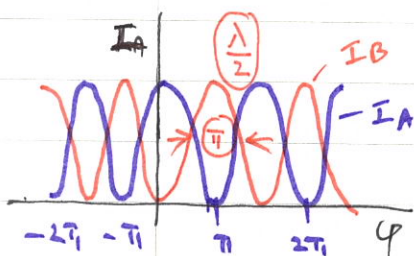
2

MZI



$$\begin{cases} I_A = \frac{I_0}{2} (1 + \cos \phi) \\ I_B = \frac{I_0}{2} (1 - \cos \phi) \end{cases}$$

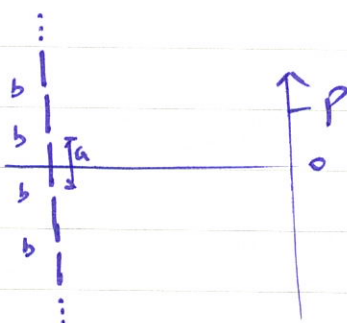
$$\begin{aligned} \cos \phi &= \cos \left(\frac{\phi}{2} + \frac{\phi}{2} \right) = \cos^2 \frac{\phi}{2} - \sin^2 \frac{\phi}{2} \\ &= 2 \cos^2 \frac{\phi}{2} - 1 \\ &= 1 - 2 \sin^2 \frac{\phi}{2} \end{aligned}$$



$$\therefore \begin{cases} I_A = I_0 \cos^2 \frac{\phi}{2} \\ I_B = I_0 \sin^2 \frac{\phi}{2} \end{cases}$$

④

Many slits

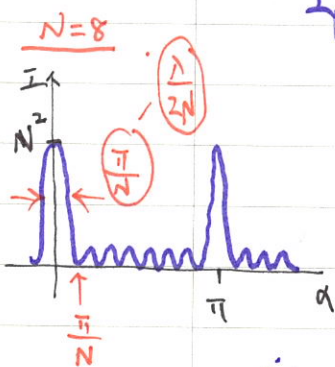


N: slit #

$$\begin{cases} \alpha = \frac{1}{2} k a \sin \theta \\ \rho = \frac{1}{2} k b \sin \theta \end{cases}$$

$$E_p = E_0 \text{sinc}(\beta) \left(\frac{\sin N\alpha}{\sin \alpha} \right)$$

$$I_p = I_0 \text{sinc}^2(\beta) \left(\frac{\sin N\alpha}{\sin \alpha} \right)^2$$

By L'Hopital's rule, $\lim_{\alpha \rightarrow m\pi} \left(\frac{\sin N\alpha}{\sin \alpha} \right) = \lim_{\alpha \rightarrow m\pi} \left(\frac{N \cos N\alpha}{\cos \alpha} \right) = N$

$$\lim_{\alpha \rightarrow m\pi} \frac{\sin N\alpha}{\sin \alpha} = \lim_{\alpha \rightarrow m\pi} \frac{N \cos N\alpha}{\cos \alpha} = N$$

$$\therefore I_p = I_0 \text{sinc}^2(\beta) N^2 \quad \text{at } \alpha = m\pi$$

For minimum, $\sin N\alpha = 0$. $\therefore N\alpha = p\pi$, $p=0, \pm 1, \pm 2, \dots$

$$\alpha = \frac{p\pi}{N}$$

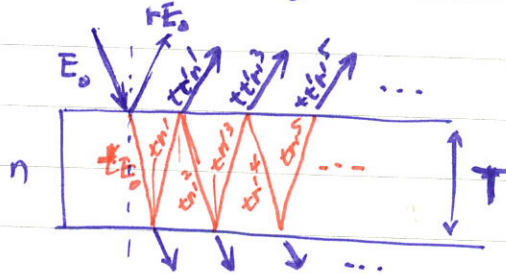
⑤

① ② ③ ④ ...

3

• Fabry - Perot

$(\sum_{j=1}^N E_j)$



• r : reflection coefficient
• t : transmission coefficient

• For reflected fields,

$$E_1 = r E_0 e^{i\omega t}$$

$$E_2 = (t t' r' E_0) e^{i\omega t} e^{-i\delta} \quad , \quad \delta = k \Delta = k 2nT \cos \theta_t$$

path length
↓

$$E_3 = (t t' r'^3 E_0) e^{i\omega t} e^{-i2\delta}$$

$$E_4 = (t t' r'^5 E_0) e^{i\omega t} e^{-i3\delta}$$

$\vdots$

$$E_R = \sum_{i=1}^N E_i = E_0 e^{i\omega t} \left(r + t t' r' \sum_{i=2}^N r'^{(2i-4)} e^{-i(i-2)\delta} \right)$$

$$= t_0 e^{i\omega t} \left(r + \frac{t t' r' e^{-i\delta}}{1 - r'^2 e^{-i\delta}} \right)$$

$x = r'^2 e^{-i\delta}$
 $x^0 + x^1 + x^2 + \dots$

By Stokes's th^m, $t t' = 1 - r^2$ & $-r' = r$ $\Rightarrow r' = -r$ $\Rightarrow r'^2 = r^2$ $\Rightarrow x = r^2 e^{-i\delta}$ $\Rightarrow |x| < 1$

$$E_R = E_0 e^{i\omega t} \left(\frac{r - r^3 e^{-i\delta} - r e^{-i\delta} + r^3 e^{-i\delta}}{1 - r^2 e^{-i\delta}} \right)$$

$$= E_0 e^{i\omega t} \left(\frac{r(1 - e^{-i\delta})}{1 - r^2 e^{-i\delta}} \right)$$

$$\therefore I_R = I_0 r^2 \left(\frac{1 - e^{-i\delta}}{1 - r^2 e^{-i\delta}} \right) \left(\frac{1 - e^{i\delta}}{1 - r^2 e^{i\delta}} \right)$$

$$= I_0 \frac{2r^2 (1 - \cos \delta)}{1 - 2r^2 \cos \delta + r^4}$$

Likewise,

$$I_T = I_0 \frac{(1 - r^2)^2}{1 - 2r^2 \cos \delta + r^4}$$

(i) For $\delta = (2m-1)\pi$, $m=1, 2, 3, \dots$
 $\cos \delta = -1$.

$$\therefore I_R = I_0 \frac{4r^2}{(1+r^2)^2} \quad \& \quad I_T = I_0 \frac{(1-r^2)^2}{(1+r^2)^2}$$

If $r \sim 1$, $I_R = I_0$ & $I_T = 0$

(ii) For $\delta = 2m\pi$, $\cos \delta = 1$.

$$I_R = \frac{0}{(1-r^2)^2} = 0 \quad \& \quad I_T = \frac{(1-r^2)^2}{(1-r^2)^2} I_0 = I_0$$

zero reflection full transmission

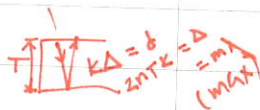
Let $F = \frac{4r^2}{(1-r^2)^2}$ & $T = \frac{I_T}{I_0} = \frac{(1-r^2)^2}{1-2r^2\cos\delta+r^4}$

→ Coefficient of Finesse

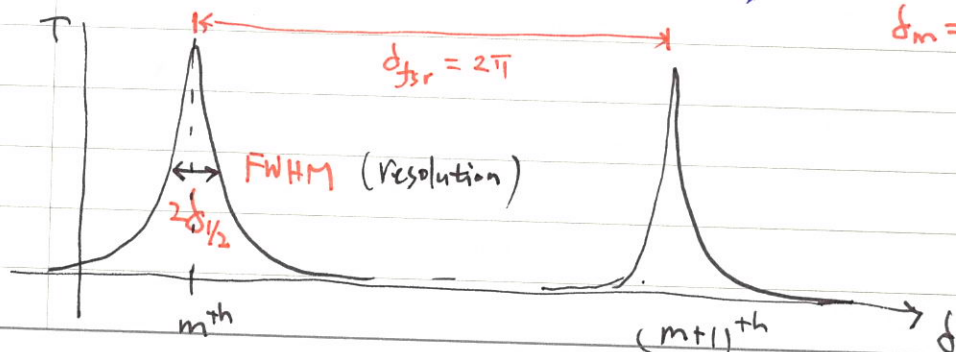
Using $\cos \delta = \cos\left(\frac{\delta}{2} + \frac{\delta}{2}\right) = \cos^2 \frac{\delta}{2} - \sin^2 \frac{\delta}{2}$
 $= 1 - 2\sin^2 \frac{\delta}{2}$

$$1 - 2r^2\cos\delta + r^4 = 1 - 2r^2\left(1 - 2\sin^2 \frac{\delta}{2}\right) + r^4$$

$$= (1-r^2)^2 + 4r^2\sin^2 \frac{\delta}{2}$$



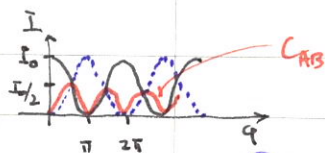
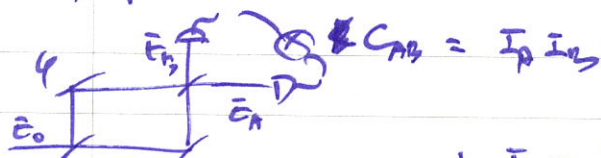
$\therefore T = \frac{1}{1 + F \sin^2 \frac{\delta}{2}}$ $F \gg 1$
Max at $\frac{\delta}{2} = m\pi$
 $\delta_m = 2m\pi$



⑥

5

Intensity product



$$I_A = \frac{I_0}{2} (1 + \cos \varphi) = I_0 \cos^2 \frac{\varphi}{2}$$

$$I_B = \frac{I_0}{2} (1 - \cos \varphi) = I_0 \sin^2 \frac{\varphi}{2}$$

$$C_{AB} = I_A I_B = \frac{I_0^2}{4} (1 - \cos^2 \varphi) = \frac{I_0^2}{4} \sin^2 \varphi$$

$$\cos 2\varphi = \cos^2 \varphi - \sin^2 \varphi = 1 - 2 \sin^2 \varphi$$

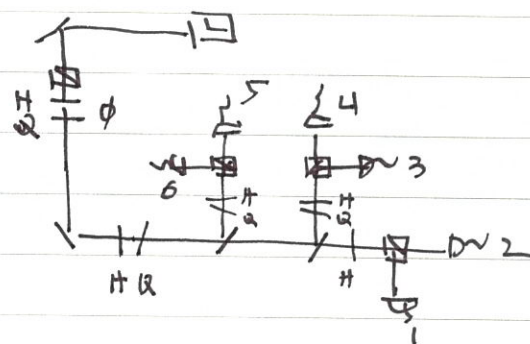
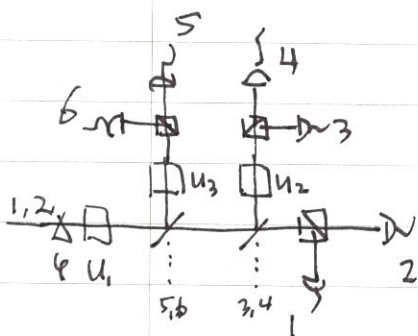
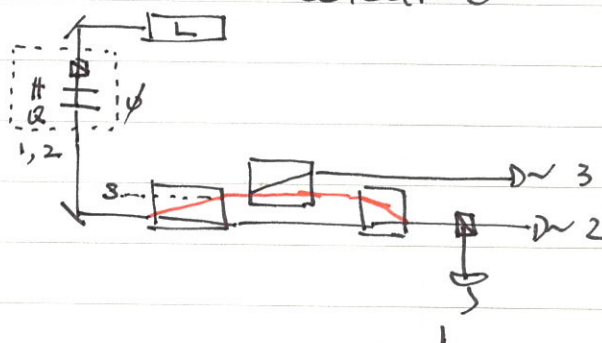
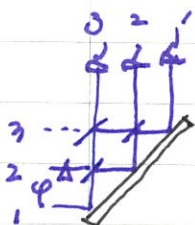
$$\rightarrow C_{AB} = \frac{I_0^2}{8} (1 - \cos 2\varphi)$$

↓ ?

$$(1 - \cos N\varphi)$$

⑦

Input mode control & output mode coincidence detection



参引. PRL 98, 223601 (07)

⑧ HAM'S way

arXiv: 2310.13217 (2023)

- Quantum eraser
- Phase control by QWP

$$\langle I_1 \rangle = \langle I_3 \rangle = \langle I_3' \rangle = \frac{I_0}{16} (1 - \sin 2\theta \cos 4\varphi)$$

$$\langle I_2 \rangle = \langle I_4 \rangle = \langle I_4' \rangle = \frac{I_0}{16} (1 + \sin 2\theta \cos 4\varphi)$$

$$\langle I_{12} \rangle = \frac{I_0}{16} (1 + \sin 2\theta \sin 4\varphi)$$

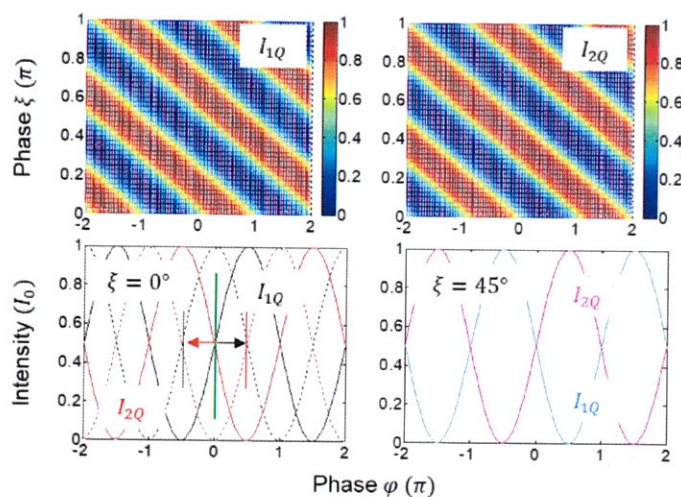
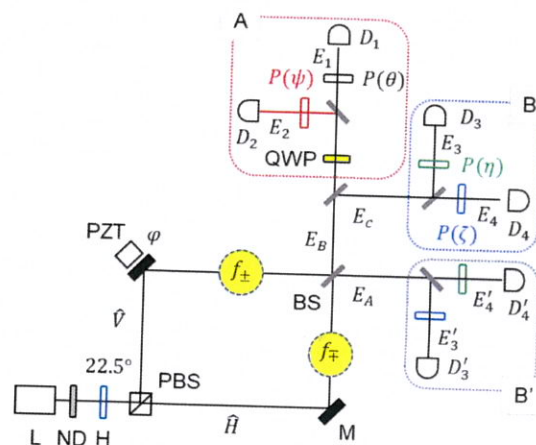
$$\langle I_{22} \rangle = \frac{I_0}{16} (1 - \sin 2\theta \sin 4\varphi)$$

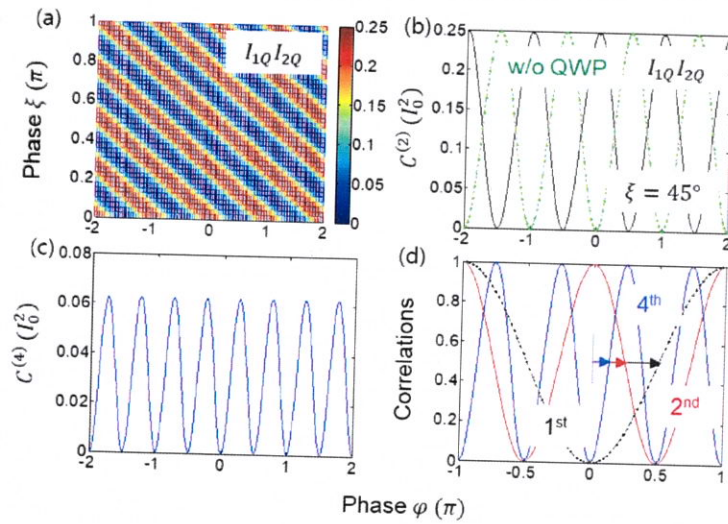
For $\theta = 45^\circ$ without QWP,

$$\begin{aligned} \text{(i)} \quad C_{AB} &= \bar{I}_A \bar{I}_B \\ &= \frac{\bar{I}^2}{16} \sin^2 \varphi. \end{aligned}$$

with QWP

$$C_{1222}(\varphi) = \frac{\bar{I}^2}{16} \cos^2 \varphi$$





Ref. PRL 98, 223601 (2007)

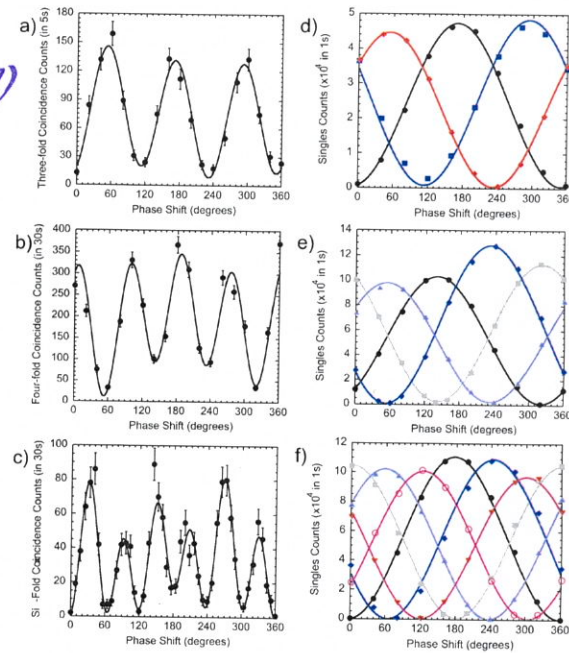


FIG. 3 (color online). (a)–(c) N -fold coincidence rates as a function of phase, ϕ , respectively, exhibiting 3, 4, and 6 distinct oscillations within a single phase cycle. The main source of uncertainty is Poissonian statistics: error bars represent the square root of the count rate. The solid line is a fit to a product of N sinusoidal fringes, as explained in the text. (d)–(f) Corresponding singles rates, each exhibiting only one oscillation per phase cycle. Error bars are contained within the data points; solid lines are the individual sinusoidal fringes obtained from (a)–(c). In (d) D1 to D3 are, respectively, indicated by black, blue, and red; in (e)–(f) D1 to D6 are indicated by black, gray, blue, cyan, red, and pink. Ideally, the phase differences between adjacent fringes is $2\pi/N$, we find: $N = 3$, $\{122^\circ, 119^\circ\}$; $N = 4$, $\{92^\circ, 90^\circ, 90^\circ\}$; and $N = 6$, $\{55^\circ, 66^\circ, 56^\circ, 62^\circ, 56^\circ\}$.